

Prediction of Breakout Noise from a Rectangular Duct with Compliant Walls

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(Received 26 June 2010, accepted 31 May 2011)

Breakout noise from HVAC ducts is important at low frequencies, and the coupling between the acoustic waves and the structural waves plays a critical role in the prediction of the transverse transmission loss. This paper describes the analytical calculation of breakout noise by incorporating three-dimensional effects along with the acoustical and structural wave coupling phenomena. The first step in the breakout noise prediction is to calculate the inside duct pressure field and the normal duct wall vibration by using the solution of the governing differential equations in terms of Green's function. The resultant equations are rearranged in terms of impedance and mobility, which results in a compact matrix formulation. The Green's function selected for the current problem is the cavity Green's function with modification of wave number in the longitudinal direction in order to incorporate the terminal impedance. The second step is to calculate the radiated sound power from the compliant duct walls by means of an "equivalent unfolded plate" model. The transverse transmission loss from the duct walls is calculated using the ratio of the incident power due to surface source inside the duct to the acoustic power radiated from the compliant duct walls. Analytical results are validated with the FE-BE numerical models.

NOMENCLATURE

		$a_n\omega$	Complex amplitude of the nth acoustic pressure mode
		$B_m(\omega)$	Structural mode resonance term
$[\mathbf{Y}_s]$	Uncoupled structural modal mobility matrix	$b_m(\omega)$	Complex amplitude of the m^{th} structural vibration velocity mode of the compliant wall
Λ_n	Normalization factor	c_0	Speed of sound in air
\mathbf{a}	Modal acoustic pressure vector	$C_{n,m}$	Coupling coefficient of the acoustic-structural mode shape
\mathbf{b}	Modal vibration amplitude vector	D	Flexural rigidity
\mathbf{g}_a	Modal force vector acting on the acoustic system	E	Young's modulus
\mathbf{g}	Generalized modal force vector due to the external force distribution	$f(\mathbf{z}, \omega)$	External force distribution on the surface of the plate
\mathbf{q}_s	Modal source vector due to vibration of the structure	h	Thickness of the duct wall
\mathbf{q}	N-length modal source strength vector	$H(\cdot)$	Heaviside function
ν	Poisson's ratio	$k = \omega/c_0$	Acoustic wave number
ω	Exciting frequency	L	Perimeter of the duct wall
ω_n, ζ_n	Natural frequency and damping ratio of the nth acoustic mode, respectively	L_1, L_2, L_3	Dimensions of the acoustic subsystem in the x_1, x_2 and x_3 coordinate directions, respectively
$\bar{\Psi}_n(\mathbf{x})$	Orthonormal function	m_1, m_2	Structural mode numbers with positive integers
$\phi_m(\mathbf{z})$	Uncoupled vibration mode shape function	n_1, n_2, n_3	Acoustic mode number integers
$\Psi_n(\mathbf{x})$	Uncoupled acoustic mode shape function	$p(\mathbf{z}, \omega)$	Acoustic pressure inside the acoustic system as function of location and frequency
ρ_0	Density of air	$p(\vec{x})$	The sound pressure inside the acoustic subsystem as function of position vector
ρ_s	Density of the duct wall material or the structural subsystem	q_n	Generalized acoustic source strength
ζ	Transverse wall displacement		
a_1, b_1	Dimensions of hypothetical piston		
$A_{m_1 m_2}$	Eigen expansion function		