

# Dynamic Behaviour Analysis of Linear Rotor-Bearing Systems using the Complex Transfer Matrix Technique

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A complex transfer matrix method is developed in the present work for analysing the steady-state response of linear rotor-bearing systems in the frequency domain. The transfer matrix of the shaft segment is derived by considering the state variables of the shaft in, a continuous system sense, to give the most general formulation. In this analysis, all the influencing parameters of the shaft, disk, and bearings are included. A three-disks-rotor-bearings system has been used as the physical model to demonstrate the effectiveness of this matrix formulation for the evaluation of the dynamic characteristics of any rotor-bearing system. In order to establish the accuracy of this technique, experiments are also conducted on the same rotor-disks model under various bearing conditions as used in the numerical analysis. The numerical results evaluated by various researchers are also compared with these experimental results.

## Nomenclature

$a, b$	– major and minor axis of elliptical whirling orbits, respectively	$M_d$	– mass of the disk
$A$	– area of cross-section	$M_x, M_y$	– bending moments about $X$ and $Y$ axes, respectively
$[B]$	– bearing matrix	$Q_x, Q_y$	– shear forces along $X$ and $Y$ axes, respectively
$C$	– bearing clearance	$r_w$	– radius of the whirl
$C_{xy}, C_{yx}$	– cross-coupled bearing damping coefficients	$[S]$	– state vectors
$C_{xx}, C_{yy}$	– direct bearing damping coefficient	$[T]$	– transfer matrix
$C_{fxx}, C_{fyy}$	– direct bearing foundation damping coefficients	$X, Y$	– displacement along $X$ and $Y$ axis, respectively
$C_{fxy}, C_{fyx}$	– cross-coupled bearing foundation damping coefficients	$\alpha, \beta$	– slopes in $X$ - $Z$ and $Y$ - $Z$ planes, respectively
$d$	– diameter of the shaft	$\alpha_t, \beta_t$	– slopes in $X$ - $Z$ and $Y$ - $Z$ planes due to shear, respectively
$D$	– diameter of the disk	$\alpha_b, \beta_b$	– slopes in $X$ - $Z$ and $Y$ - $Z$ planes due to bending, respectively
$D_b$	– diameter of the bearing	$\omega, \Omega$	– rotating and whirling speeds, respectively
$[D]$	– disk matrix	$\rho$	– mass density
$e(x), e(y)$	– eccentricity of the disk in $X$ and $Y$ directions, respectively	$\mu$	– coefficients of viscosity
$E$	– Young's modulus of rotor		
$EI$	– bending stiffness	<b>Subscripts</b>	
$G$	– shear modulus	$C, S$	– associated to cosine and sine terms, respectively
$h$	– disk thickness	$0, n$	– stage number
$I_d, I_p$	– transverse and polar mass moments of inertia of the disk, respectively	<b>Superscripts</b>	
$j$	– imaginary unit	$L, R$	– left and right to the station, respectively
$I, J$	– transverse and polar area moments of inertia of the rotor, respectively	$t$	– transpose of the array
$K_s$	– form factor		
$K_{xy}, K_{yx}$	– cross-coupled bearing stiffness coefficients		
$K_{xx}, K_{yy}$	– direct bearing stiffness coefficients		
$K_{fxx}, K_{fyy}$	– direct bearing foundation stiffness coefficients		
$K_{fxy}, K_{fyx}$	– cross-coupled bearing foundation stiffness coefficients		
$l$	– length of the rotor segment		
$L_b$	– length of the bearing		
$m$	– mass of the rotor segment for unit length		
$m_b$	– mass at the supported bearing		
$m_e$	– mass of the unbalance		

## 1. INTRODUCTION

The transfer matrix method (TMM) can be used to solve dynamic problems in the frequency domain, which makes it suitable for analysing the steady-state responses of rotor-bearing systems with satisfactory accuracy. The TMM was first applied to a rotor-bearing system by Prohl,<sup>1</sup> who considered rigid bearing characteristics and four state variables. However, subsequently, this concept has been modified by incorporating the dynamic characteristics, such as stiffness and damping coefficients of fluid-film bearings, into the analysis. Kikuchi<sup>2</sup> and Lund<sup>3,4</sup> made a significant advancement by including the effects of gyroscopics, internal friction,